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Screening of Oil Pools on Alaska North Slope and Phase Behavior Study of Viscous Oil and CO₂ System in Conjunction with CO₂ Sequestration

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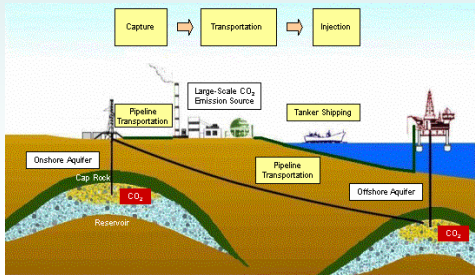
Anchorage, AK
October 1, 2008



Introduction

Global Warming and Arctic Environment

- Increase in average winter temperature
- Reduction in the extent of the summer ice pack in the Arctic Ocean
- Either change could accelerate warming
- Change could substantially reduce winter drilling window, thus threatening oil and gas developmental drilling and related activities




The diagram illustrates the process of CO₂ capture from a 'Large-Scale CO₂ Emission Source', followed by 'Transportation' via 'Pipeline Transportation' and 'Tanker Shipping'. The CO₂ is then 'Injected' into 'Onshore Aquifer' and 'Offshore Aquifer' geological formations. A 'Cap Rock' is shown above the reservoir, and a 'Reservoir' is shown below. The diagram also shows an oil rig on the offshore aquifer.

Why Geological Sequestration?

- CO₂ is an important GHG gas
- Geological formation has potential
- Experience from the oil and gas industry
- Global storage capacity is around 24 gigatons

Source: <http://www.irccm.de/greenhouse/files/greenhouse06.png>

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Introduction (cont'd)

Why store CO₂ in Alaska?

- Arctic: impact of climate change is more pronounced
- Viscous oil production by CO₂ flooding
- IEA estimates 6000 SCF CO₂ stored for 1 STB of oil (Fanchi, 2001)
- Annual CO₂ generation on North Slope

Gas turbines + handling facilities = 14 million tons

Gas sales = 8 million tons

TOTAL = 22 million tons

Necessity: Advances in drilling technology to develop engineered well bores to avoid communication between injected CO₂ and producer wells.

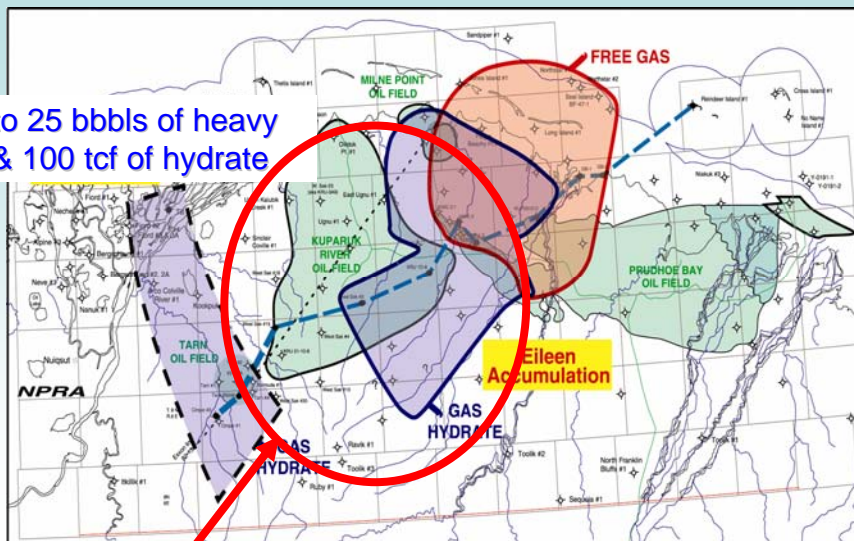
Benefits: Increased oil and gas production in an environmentally friendly manner, leading to economic development.

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FOSSIL ENERGY RESOURCES AT STAKE

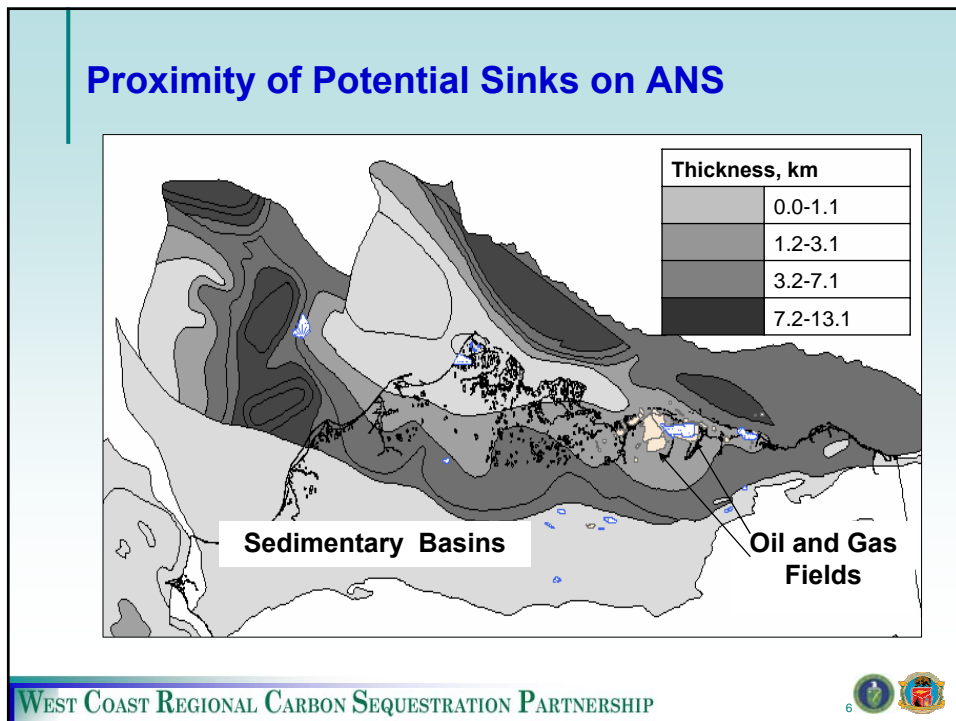
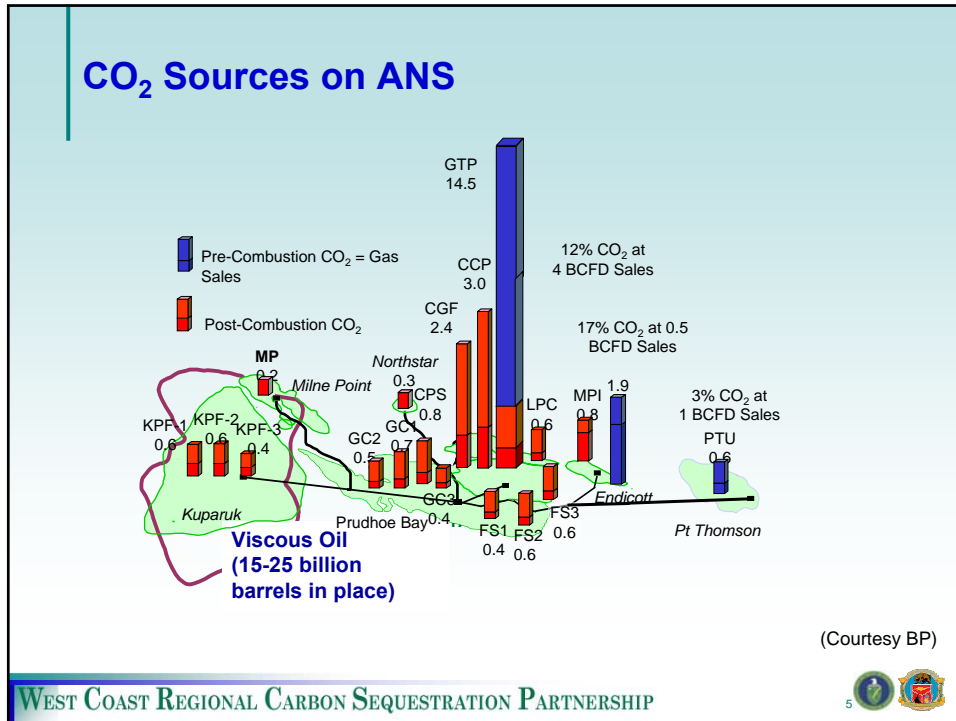
Upto 25 bbbbls of heavy oil & 100 tcf of hydrate

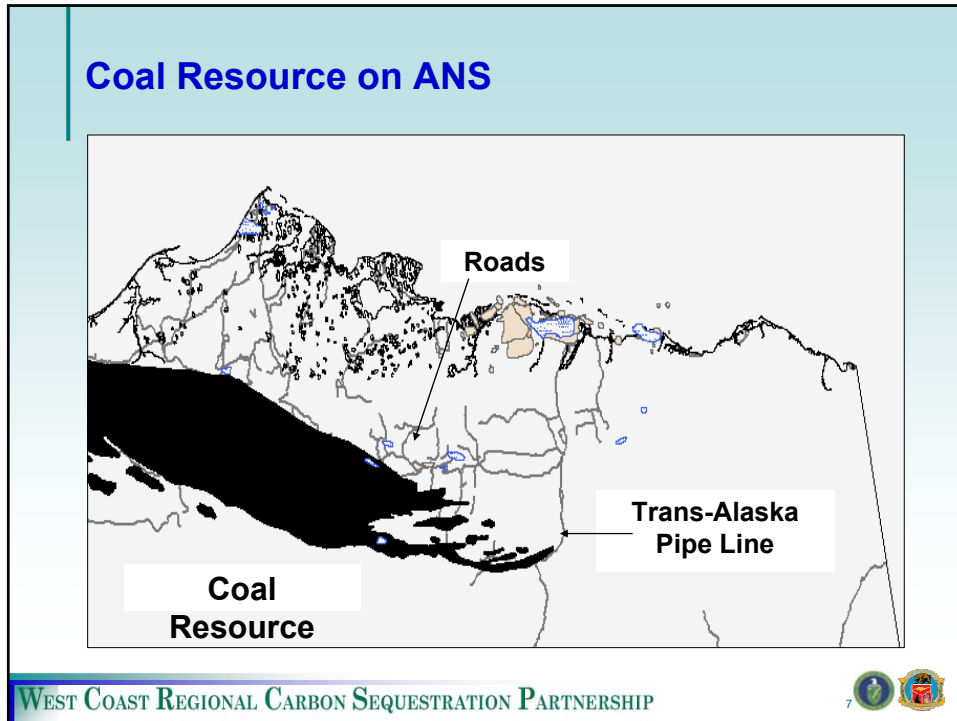


Viscous Oil and Gas Hydrate Resource Focus Area

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- ### Objectives of the Study
- Characterize oil pools, amenable to CO₂-EOR, on ANS by parametric screening technique
 - Simulate phase behavior by tuning Equation-of-State
 - Prediction of oil production by CO₂ injection with compositional simulator as well as related economics
 - Study of long-term CO₂ storage in a saline aquifer
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Screening of Oil Reservoirs

- Influencing parameters for CO₂-EOR studies:
Temperature, Pressure, Porosity,
Permeability, API gravity, Oil saturation,
Minimum Miscibility Pressure (MMP),
and Net pay zone thickness
- Parametric study is adopted – Optimum values of above factors are considered to screen out reservoirs best for EOR



Rank (R_i) of the ANS Oil Pools

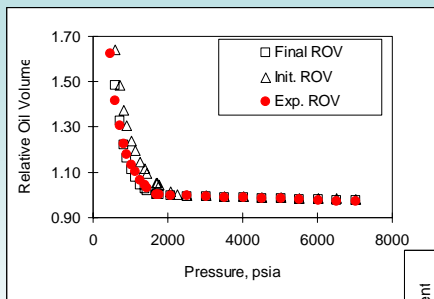
Pool	T, °F	Φ, %	k, md	S _o , %	h, ft	° API	P/ MMP	R _i
Pt. McIntyre	180	22	200	60	156	27	1.27	1
Meltwater	140	20	10	60	95	36	1.5	2
Lisburne	183	10	1.5	70	125	27	1.03	3
Tarn	142	20	9	60	40	37	1.64	4
Prudhoe	200	22	265	70	222	28	0.94	5
Alpine	160	19	15	80	48	40	1.81	6
Kupurak -Milne	160	20	150	90	100	24	0.79	7
Kupurak River	165	23	40	70	35	22	0.76	8
Sag River	234	18	4	60	30	37	1.86	9
North Prudhoe	206	20	590	60	20	35	2.07	10
West Sak	75	30	1007	70	70	19	0.41	11
Schrader Bluff	80	28	505	70	70	17.5	0.4	12
Hemlock	180	10.5	53	70	290	33.1	2.34	13
Ivishak	254	15	200	50	125	44	4.11	14



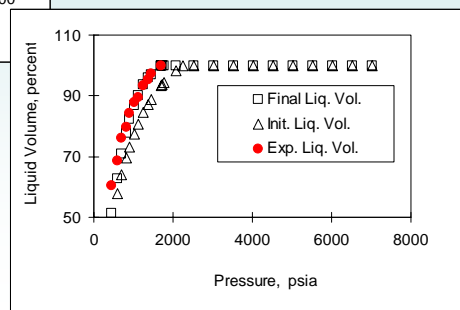
Phase Behavior Study

- The phase behavior of any reservoir fluid in CO₂ injection involves mass transfer and changes in composition.
- Any compositional simulator can predict the phase behavior of gas flooding, provided the Equation-of-State (EOS) is tuned.
- In the case of West Sak oil, the phase behavior during CO₂ injection was used to estimate the miscibility condition

Results after Regression



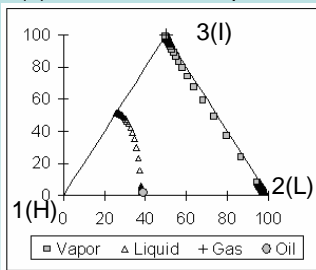
Better match of ROV and % liquid volume after Regression



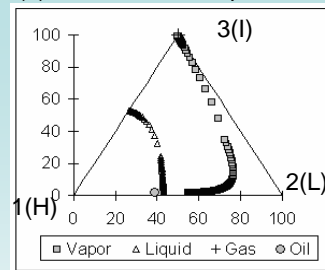
Multiple Contact Miscibility—CO₂ Injection

- To investigate the miscibility condition for the mixture of West Sak crude and 100% CO₂, the miscibility prediction were obtained by using tuned PR-EOS
- Pseudo-ternary diagrams are used to describe for West Sak crude in CO₂ injection process

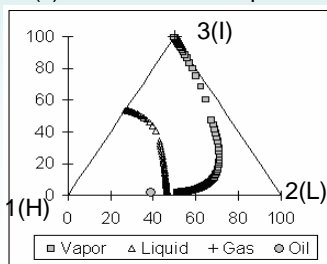
(a) Pressure =1600 psia



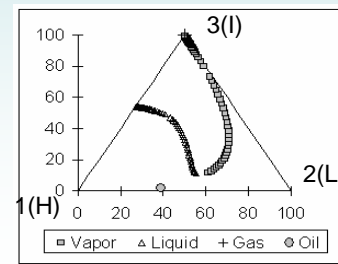
(b) Pressure =2600 psia



(c) Pressure = 3600 psia



(d) Pressure =6600 psia

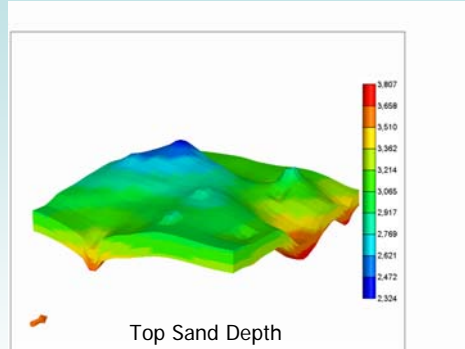


Component 1: C7+ as the heavy fraction (H)
Component 3 : C2,C3,C4,C5,C6,CO2 as the intermediate fraction (I)

Component 2: N2,C1 as the light fraction (L)

West Sak Reservoir and Properties

Area around 260 sq. miles
Oil gravity 14–22.5 API
Porosity up to 38%
Permeability 10–140 md

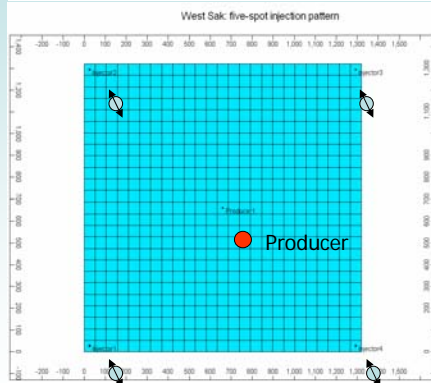


Drawn using well log data by Panda et al. (1988) and geostatistical tool

Due to the vast nature of the West Sak Pool, only small portion of the reservoir was selected for the simulation study

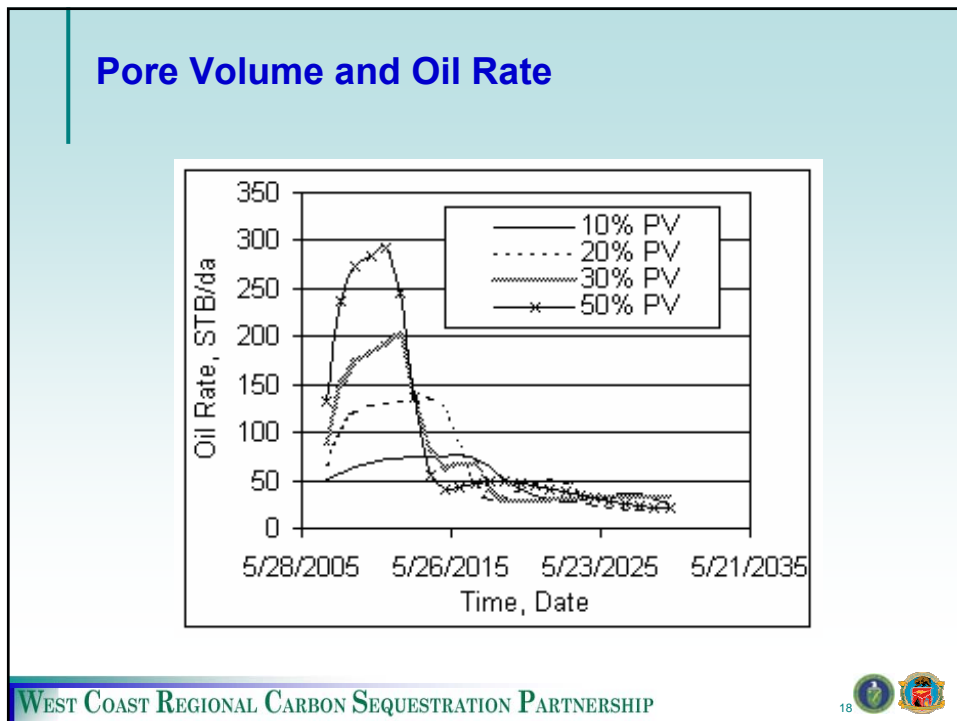
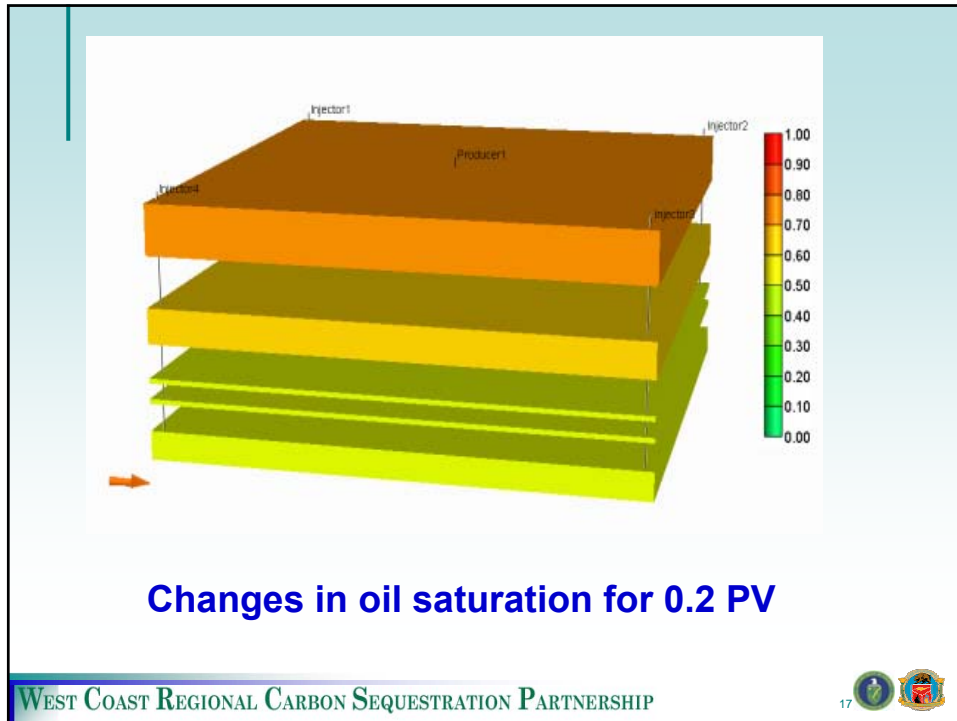
Injection Pattern in CMG's GEM (Compositional Model)

West Sak five-spot CO₂ injection pattern

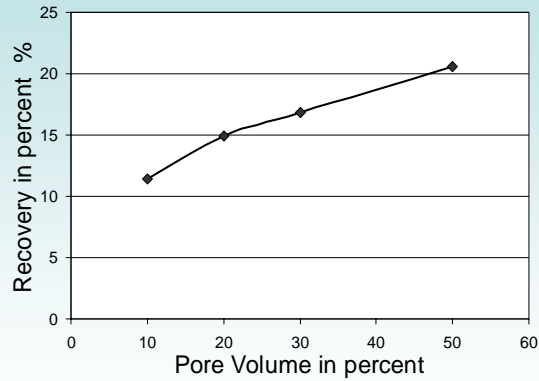


- Five sand layers separated by shale layers
- Avg. petrophysical properties were obtained from Bakshi (1991)
- Previously tuned equation-of-state was put into the model
- CO₂ was continuously injected into the reservoir for 24 years

25 x 25 x 9 Cartesian model: 40 acre area



Pore Volume and Oil Recovery for 24-Year CO₂ Injection



Increase in injection pore volume increased the oil rate and % recovery (OOIP= 4.015MM STB), but it led to early onset of breakthrough

Summary of Injection at 24-Year Period

% PV	% Recovery	CO ₂ Injected, million standard cubic ft	CO ₂ Produced, million standard cubic ft	CO ₂ Storage Ratio
10	11.40	1.598	0.075	0.95
20	14.93	3.196	1.009	0.68
30	16.82	4.841	2.327	0.52
50	20.62	8.040	4.981	0.38

For 50% pore volume of CO₂ injection was found to be 9.709 Mscf/STB of oil produced

Oil production and corresponding CO₂ storage for 0.5 PV was considered for economical modeling for CO₂-EOR

Economic Model

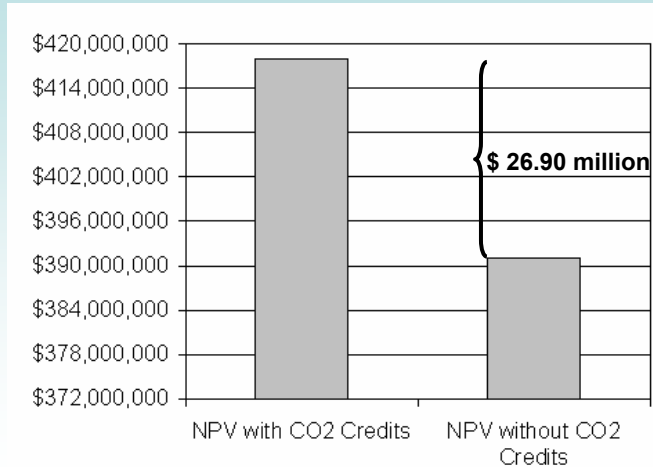
- To evaluate the feasibility of the CO₂ sequestration with EOR
- Costs for each stage of the CO₂-EOR project includes
 - CAPEX: Capital Expenditures
 - OPEX: Operating Expenditures
- Annual net cash flow (NCF), as given by Gasper et al. (2005), was used to calculate the net present value (NPV) of the EOR project
- $NCF = (\text{Gross Revenue} + \text{CO}_2 \text{ credits} - \text{Royalty} - \text{OPEX} - \text{Annual drilling or completion cost (if any)} - \text{Depreciation}) \times (1 - \text{Corporate tax}) + \text{Depreciation} - \text{CAPEX}$

Economic Model

- 40 X 75 (3000) acre area to justify the construction of pipeline as well as CO₂ compression unit and other facilities
- Stored CO₂ will be 75 times the 40 acre flood pattern = 1.37 million tons per year for 50% PV scenario

Parameter	Assumed Value for NPV
Oil Price (US \$/bbl)	50
Project Life (years)	25
Royalty	12.50%
Corporate Tax	35%
Discount Rate	12%
Rent	\$12/acre
Storage Ratio	38 %
CO ₂ Credits (US \$/ton CO ₂)	10
Capture Cost (US \$/ton CO ₂)	3
Compression Cost (US \$/tonCO ₂)	7.5
Transportation Cost (US \$/ton CO ₂)	8
Storage Cost (US \$/ton CO ₂)	3

Comparison of NPV



Increasing with CO₂ in terms of PV can lead to more NPV with CO₂ credits as long as no leakage conditions are present

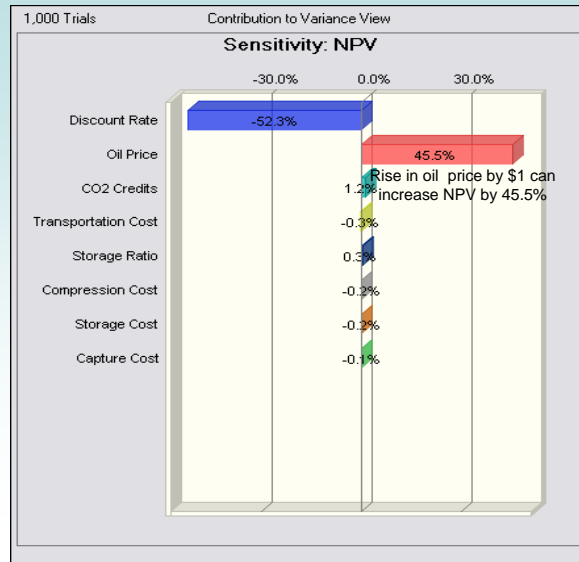
Economic Model

Parameters for Sensitivity Analysis

Variable	Distribution	Parameter Values
Discount Rate	lognormal	Mean = 12%; standard deviation = 4%
Oil Price	lognormal	Mean = 50; standard deviation = 10
CO ₂ Credits	lognormal	Mean = 10; standard deviation = 5
Storage Cost	triangular	1.5; 3; 4.5
Capture Cost	triangular	1.5; 3; 4.5
Compression Cost	triangular	6; 7.5; 9
Storage Ratio	normal	Mean = 37%; standard deviation = 10%
Transportation Cost	triangular	6; 8; 10

Source: Gaspar et al. (2005)

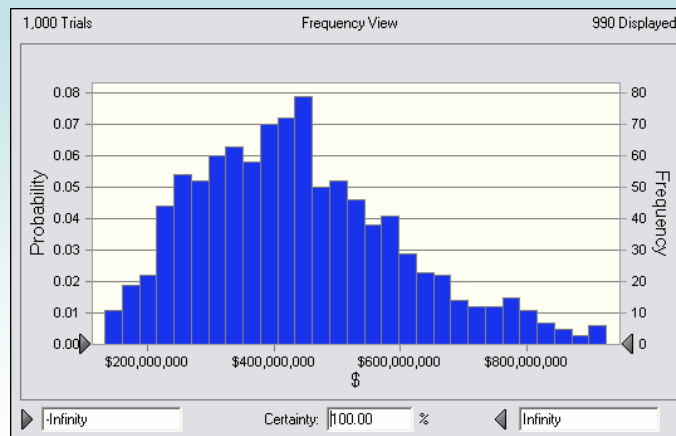
Sensitivity Analysis of NPV Using Monte Carlo Simulation



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Probability Distribution



Probability distribution shows mean of the NPV would be around US\$0.44 billion

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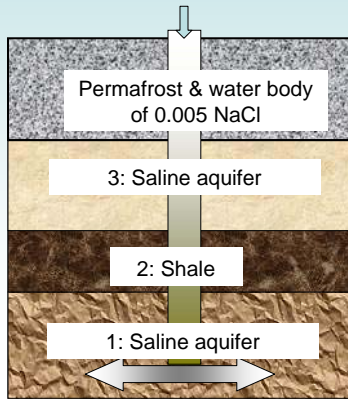
Use of STOMP-WCSE

CO₂ injected was injected in the bottom layer for 10 years (3650 days): 4.4 lb/s

Purpose: To study temperature profile and its impact on CO₂ solubility

2-d 42 by 28 radial model

Properties of CO₂ at 45°C



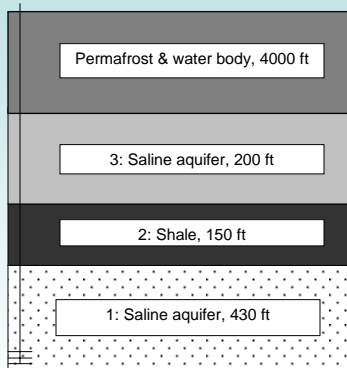
	P (bar)	120	160
fluid phase			
pure water			
density (kg/m ³)		994.768	996.292
viscosity (Pa s)		5.97778e-4	5.98341e-4
water with CO₂			
density (kg/m ³)		994.768	996.292
viscosity (Pa s)		5.97778e-4	5.98341e-4
CO ₂ mass fraction		5.22541e-2	5.70921e-2
gas			
density (kg/m ³)		658.574	760.891
viscosity (Pa s)		5.16820e-5	6.56320e-5
water mass fraction		9.93985e-5	8.60323e-5

Source: PNNL

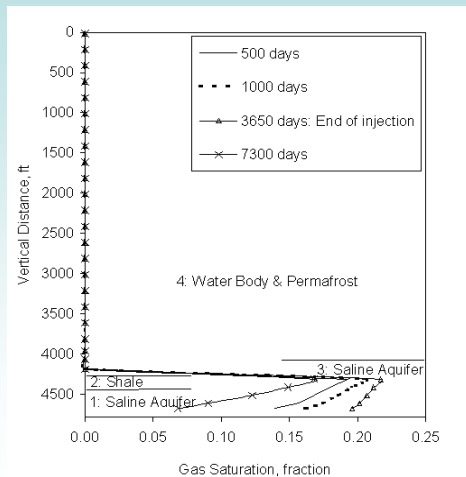
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Results of CO₂ Injection Studies



Two-dimensional cylindrical model used in Subsurface Transport Over Multiple Phases@-Water-CO₂-NaCl-Energy (STOMP@-WCSE).

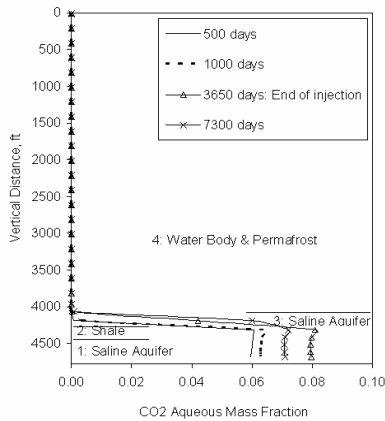


Gas saturation at a horizontal distance of 280 ft from the injection well.

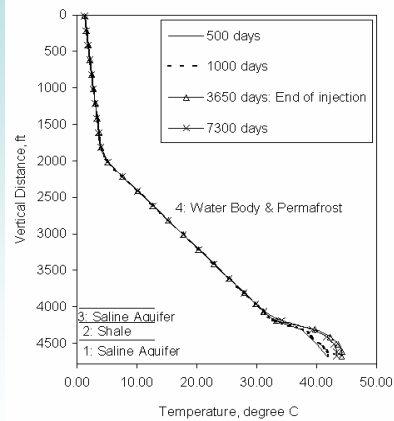
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Results of CO₂ Injection Studies (cont'd.)



CO₂ aqueous fraction at a horizontal distance of 280 ft from an injection well



Temperature profile at a horizontal distance of 280 ft from an injection well

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Conclusions

- Weight-assigned parameters such as temperature, pressure, and average petrophysical properties of the oil pools are important in carrying out rudimentary screening of potential oil pools on the ANS with respect to their amenability to CO₂-EOR.
- At the reservoir pressures typical of the West Sak oil pool, the presence of partial miscibility can be determined through phase-behavior study.
- Oil recovery by continuous CO₂ injection for 25 years predicted 20.62% oil recovery when 50% PV of CO₂ was injected. An increase in PV led to a decrease in CO₂ storage ratio.
- Economic analysis of CO₂-EOR proved to be important in estimating the time value of the project. The NPV of the project with CO₂ credits was found to be higher by US\$26.90 million than NPV without CO₂ credits.
- At a rate of 4.40 lb/sec, a saline aquifer can successfully sequester CO₂ with no leakage. Changes in the temperature profile were negligible when supercritical CO₂ was injected in a saline formation with a NaCl mass fraction of 0.05.

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